

# Human Exploration of Earth's Neighborhood and Mars



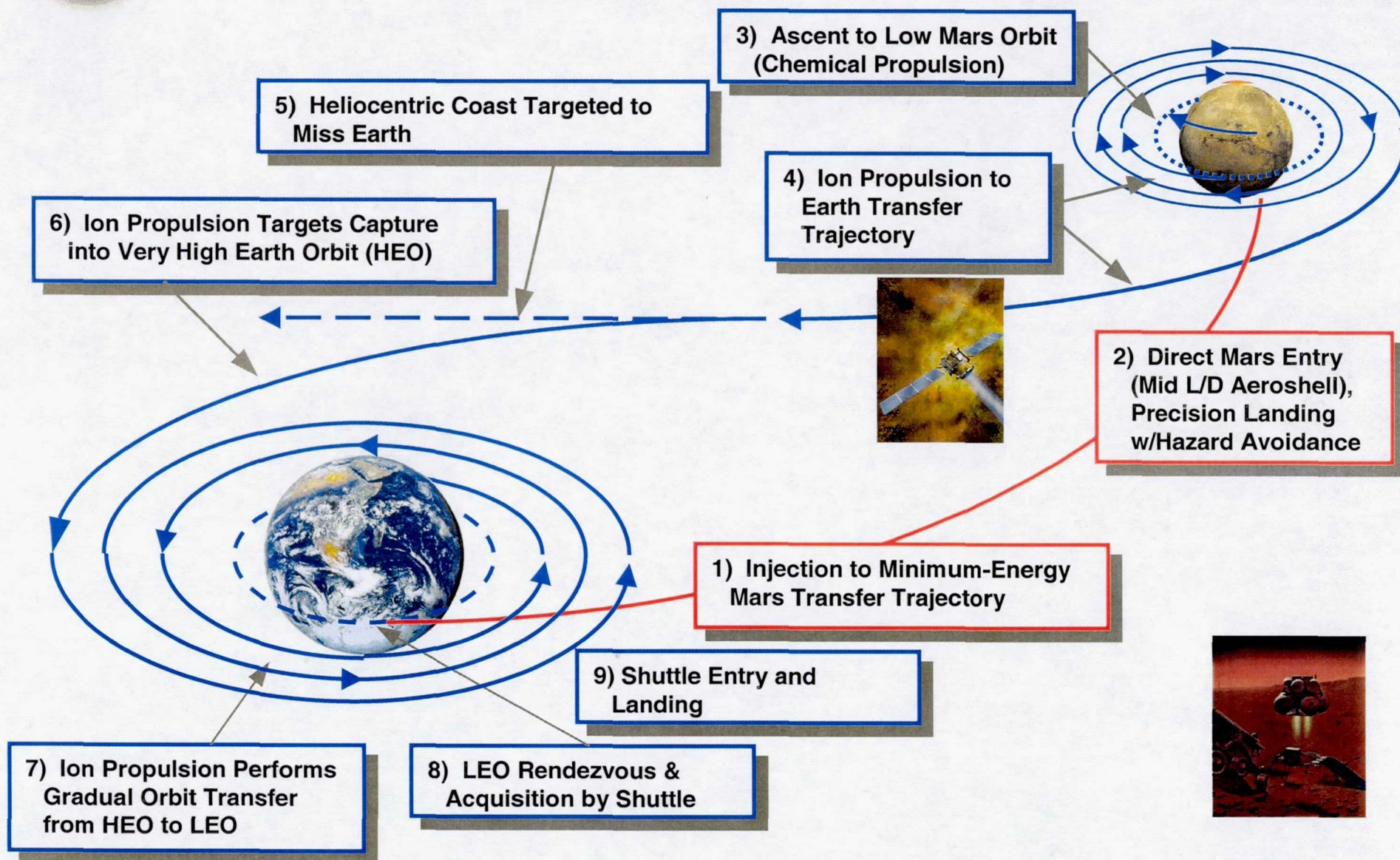
Jerry Condon / JSC/EG5 / 281-483-8173 / [gerald.l.condon1@jsc.nasa.gov](mailto:gerald.l.condon1@jsc.nasa.gov)





# Mission Scenario

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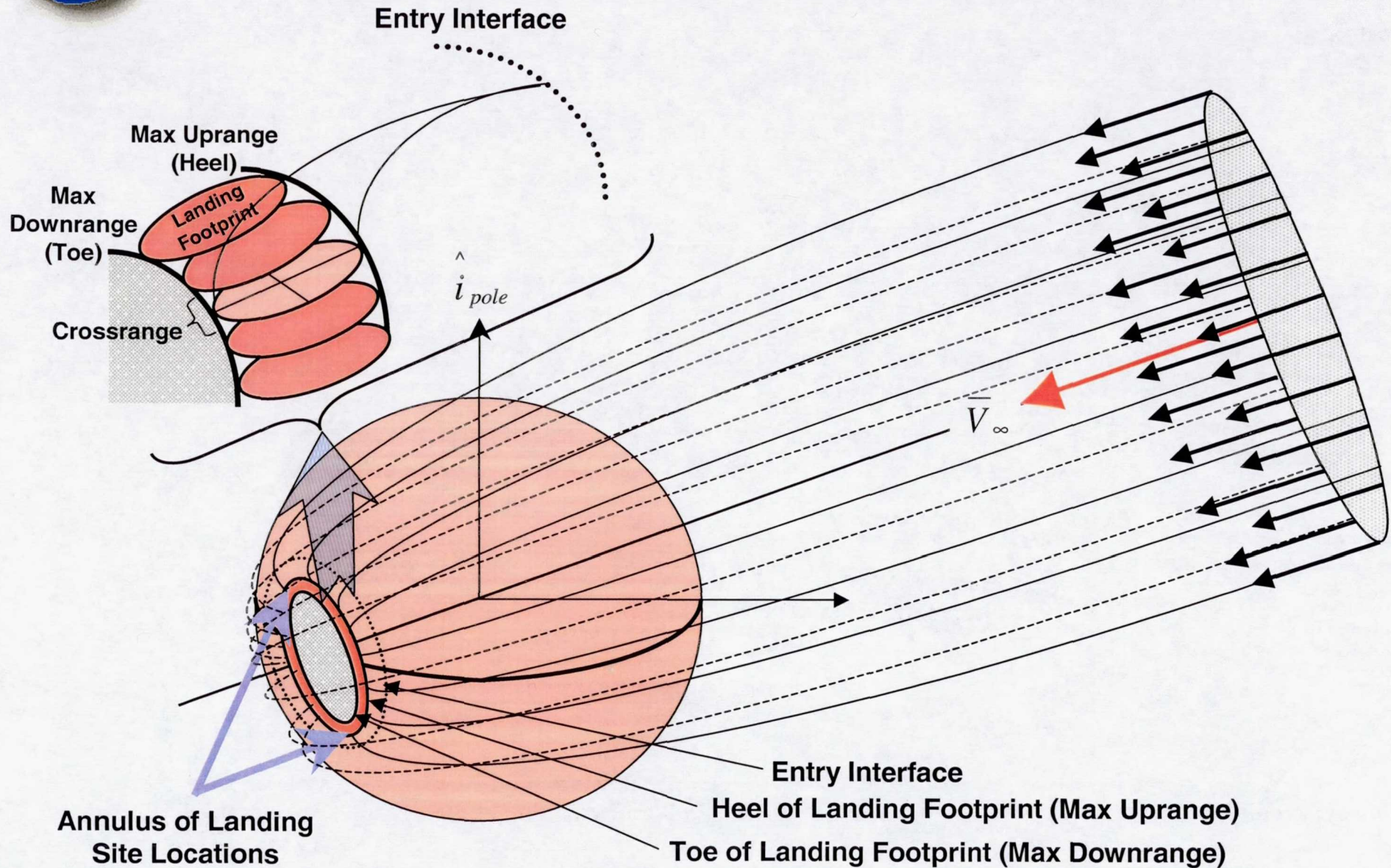






# Direct Entry Landing Locations

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## 2005 Opportunity - Type I

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### 2005 Opportunity

Type I

Earth Departure Date

8/10/05

Earth Departure Energy

$C3 = 15.9 \text{ km}^2/\text{s}^2$

Mars Arrival Date

2/25/06

Trip Time

199 days

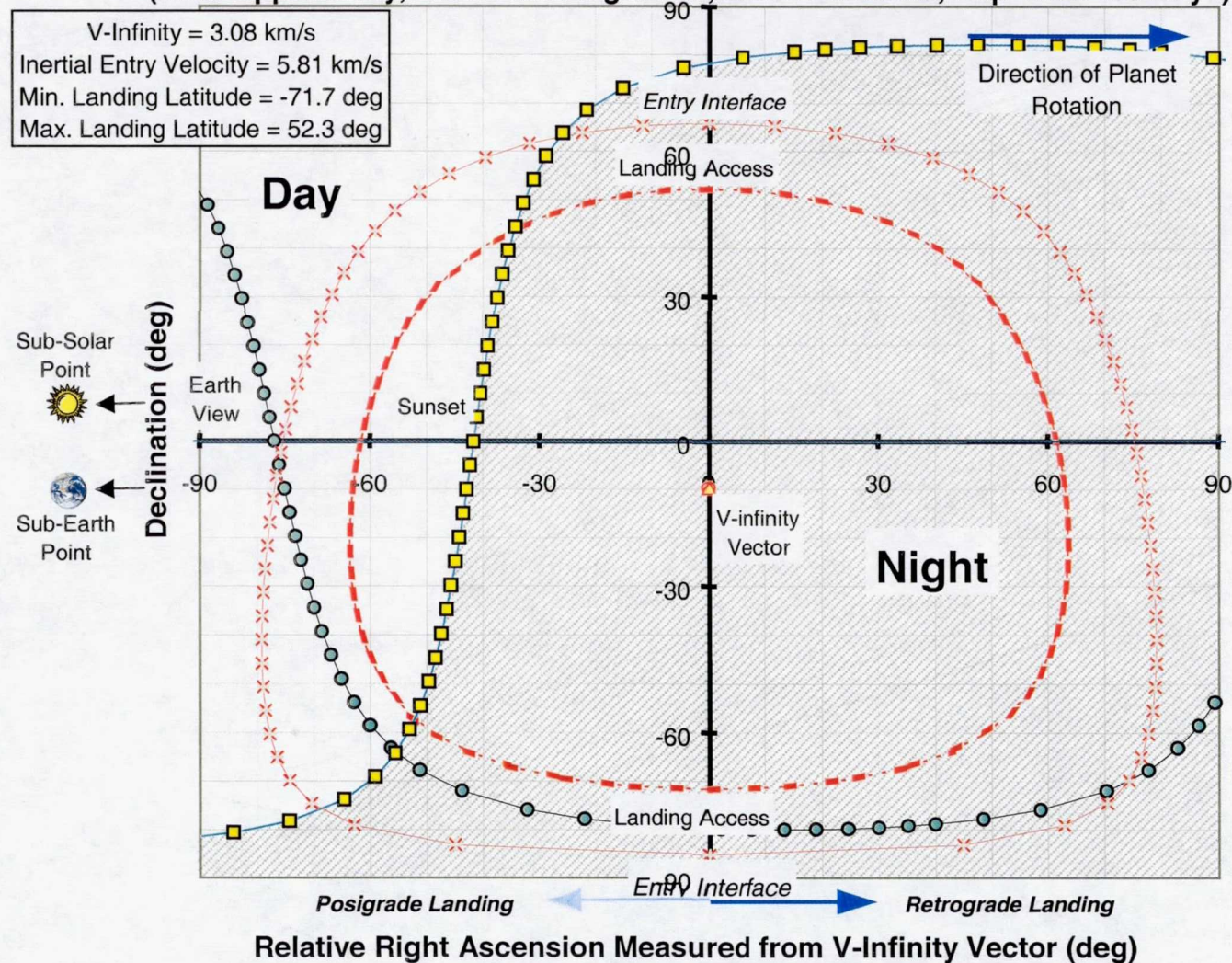
Mars Inertial Entry Speed

5.81 km/s

Landing Site Latitude Access

$-71.7^\circ \rightarrow 52.3^\circ$

### Landing Lighting and Latitude for Direct Entry JSC Mars Sample Return (2005 Opportunity, Date/Time August 10, 2005 12:00:00.0, Trip Time 199 Days)

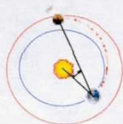




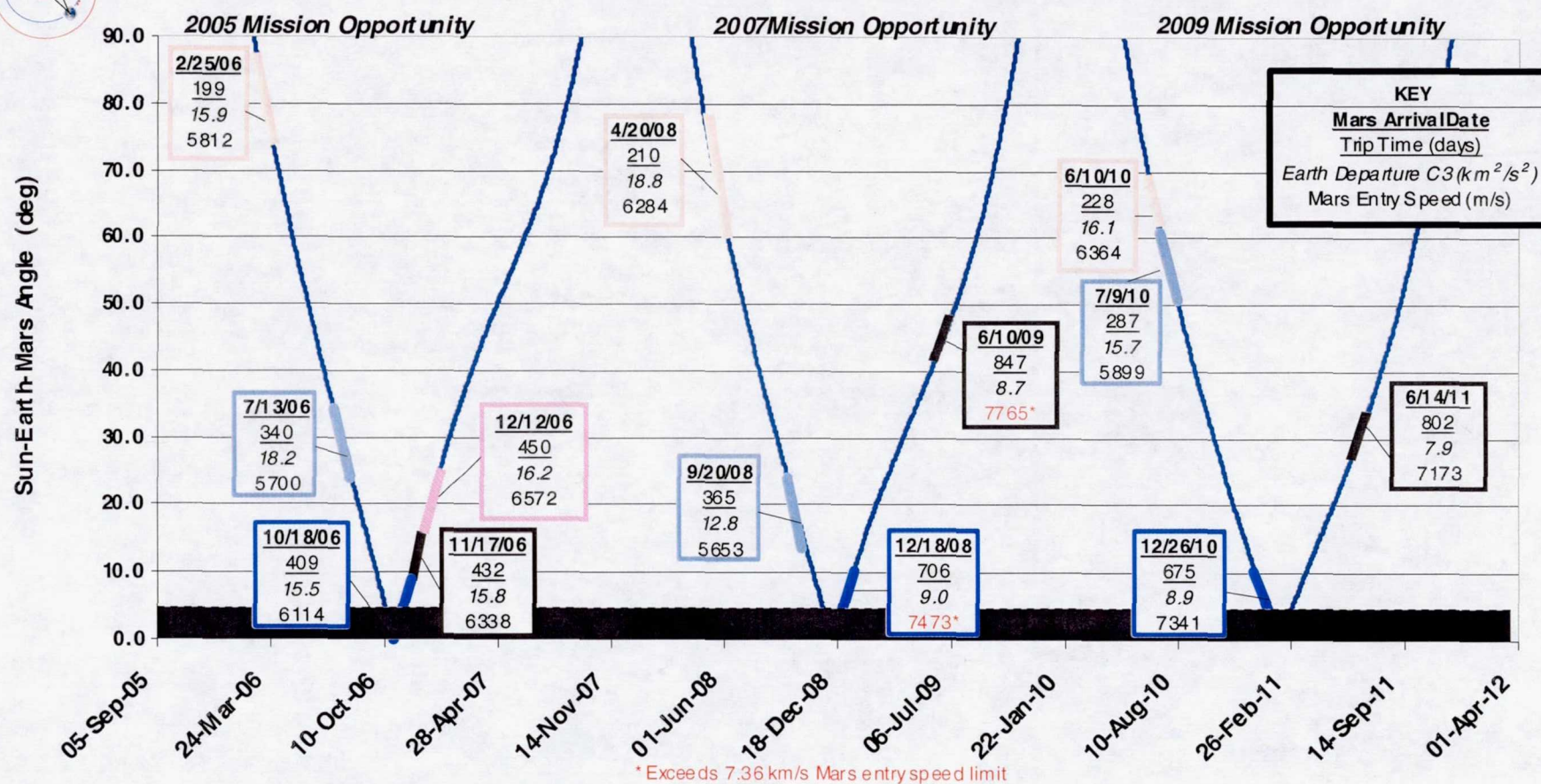


# Earth-Mars Superior Conjunction

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## Earth-Mars Superior Conjunction

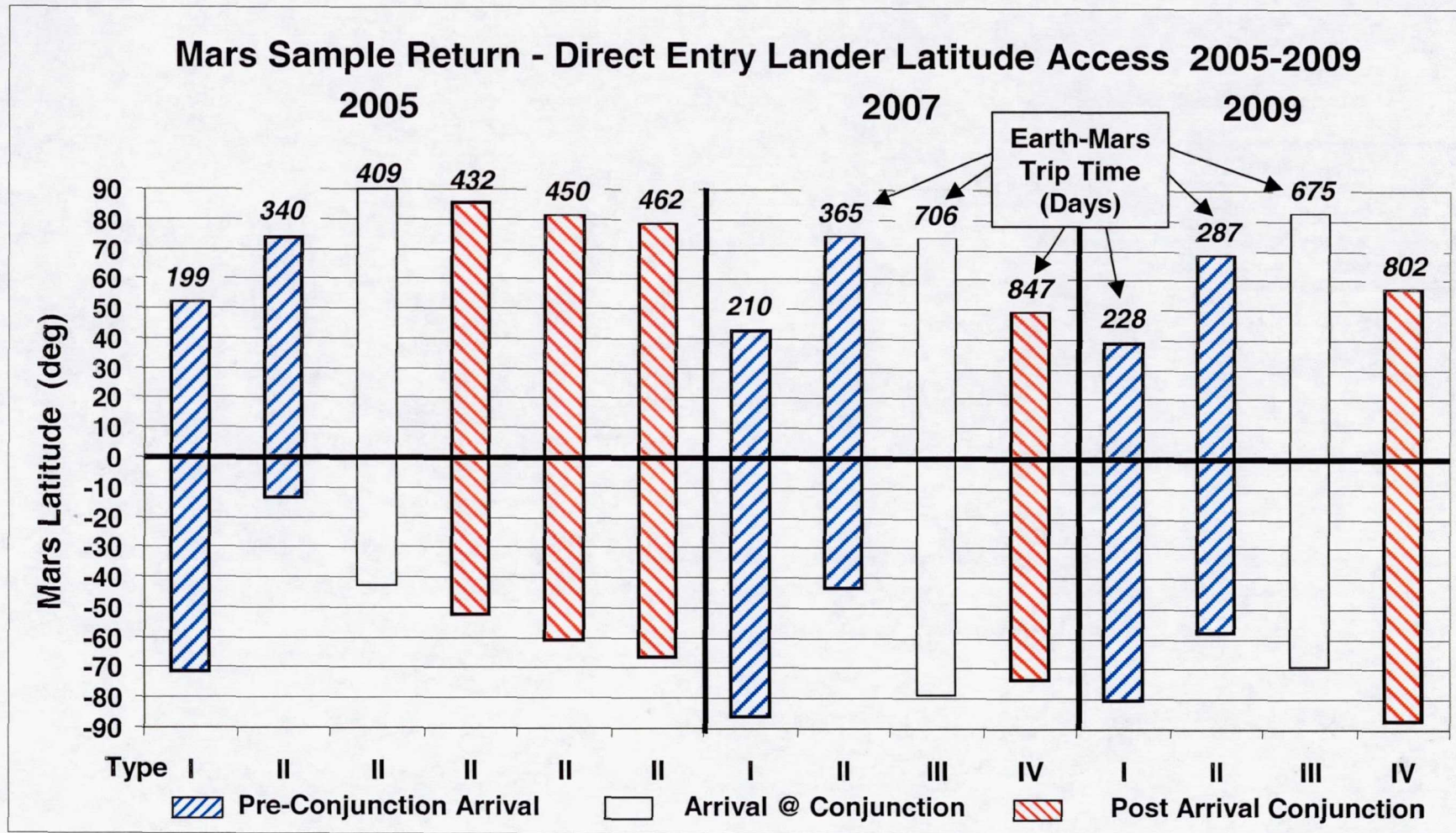






# Lander Latitude Accessibility

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## Low Thrust – Earth Return Phase

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- Two-body assumption with mass-matching at transition points, no shadowing
- Initial Conditions\*
  - Mass = 350 kg
  - Power to thruster = 2.567 kW
  - Efficiency = 55.3%
  - Isp = 3127 sec.



\*Based on advanced NSTAR engine similar to that used with Deep Space 1





# SEP Earth Return Sequence

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## Mars Spiral Out

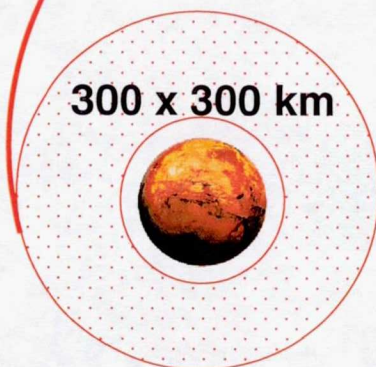
- Depart 300 km circular parking orbit
- Initial mass = 350 kg
- Thrust along velocity vector
- Spiral to zero energy condition
- No shadow
- **Transfer Time = 131 days**
- **Propellant = 34 kg**

## Earth 'Spiral' Down

- Depart 150,000 x 20,000 parking orbit
- Apogee Reduction to 20,000 km
  - Thrust perpendicular to line of apsides near perigee
- Spiral down to 500 km circular orbit
  - Thrust opposite velocity vector
- Preliminary 60 kg estimate for spiral down propellant (later optimized to 38 kg)

Coast

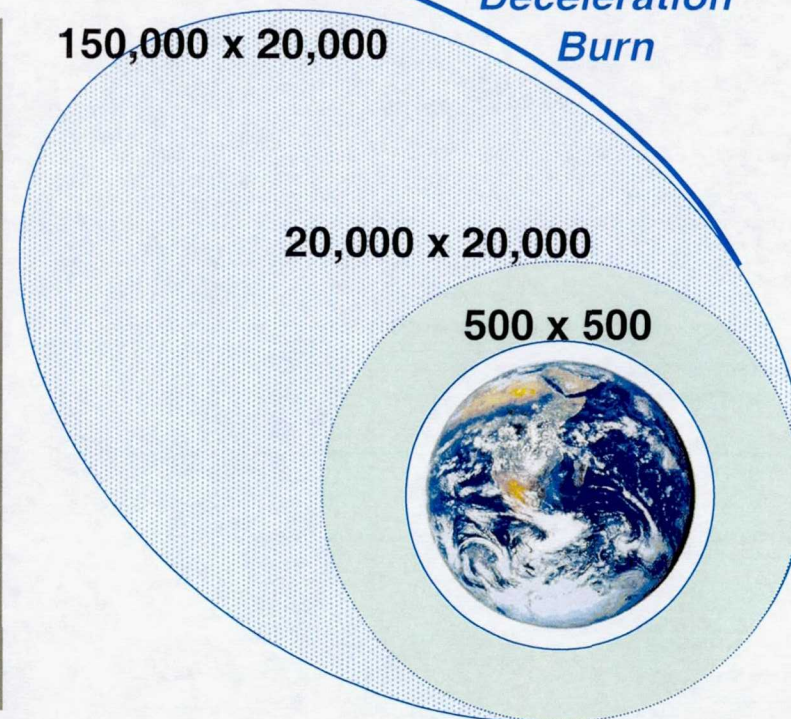
**Acceleration  
Burn**



## Heliocentric Transfer

- Depart Mars state
- Initial mass = 316 kg
- Optimal thrust direction (Calculus of Variations)
- Capture to a 150,000 x 20,000 km parking orbit
- **Transfer time = 370 to 490 days**
- **Required mass in LEO > 200 kg**
  - Assumes 60 kg propellant required to capture into HEO and spiral down to LEO

**Deceleration  
Burn**



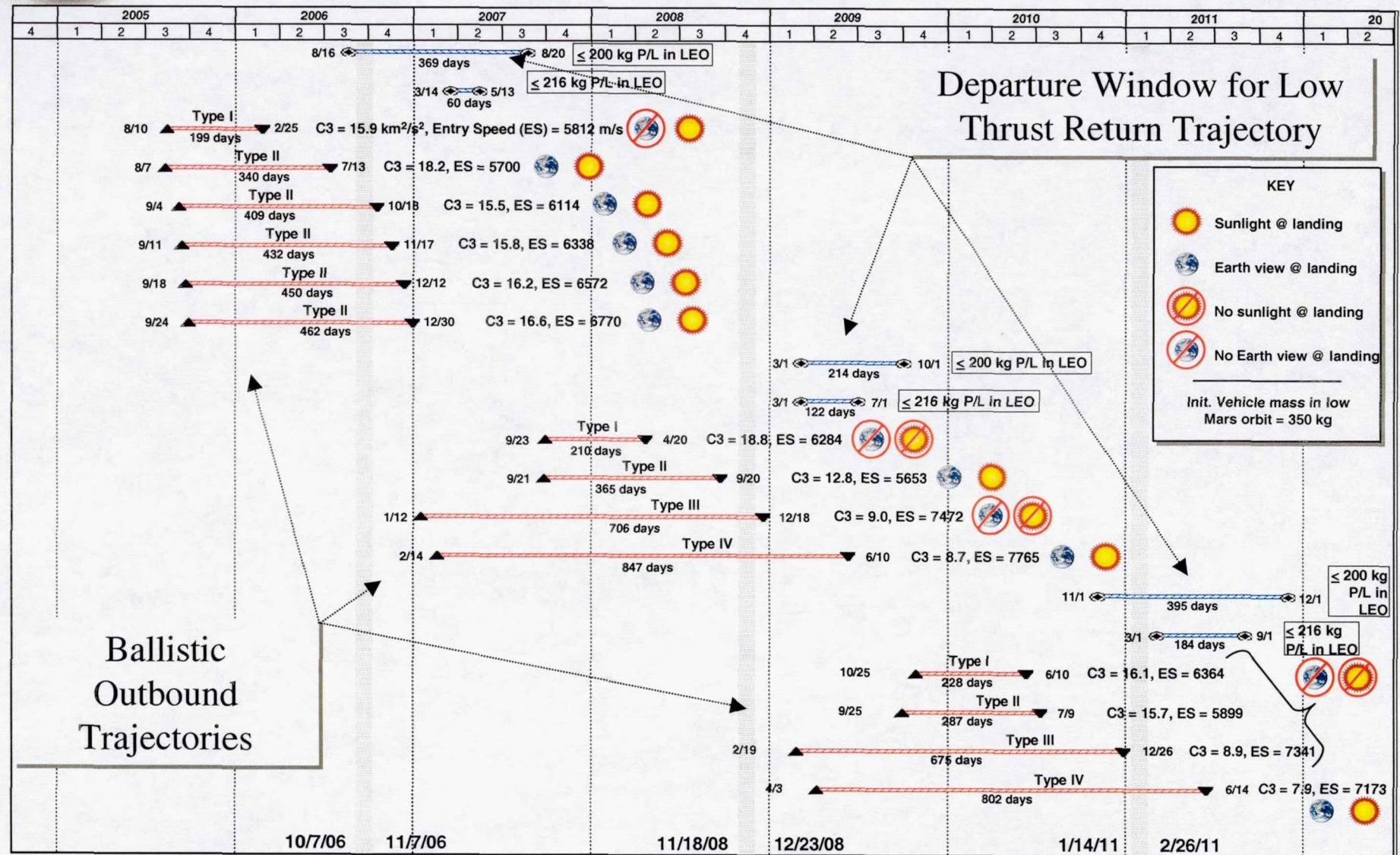




# Missions – 2005, 2007, 2009

Ballistic Outbound Trajectories and Mars Low Thrust Return Departure Window

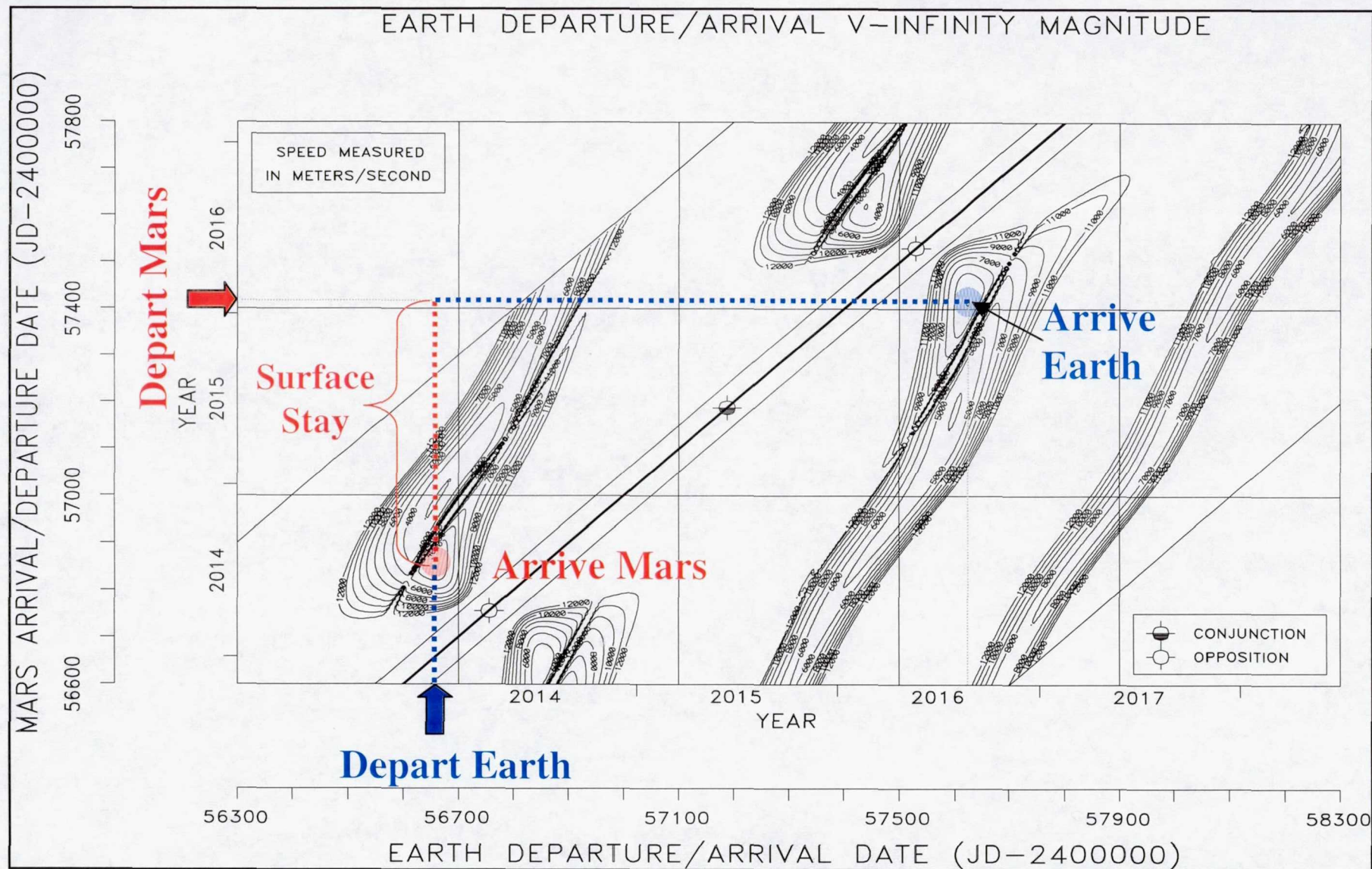
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# Mission Map







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# EARTH TO MOON TRANSFERS

## DIRECT VS VIA LIBRATION POINTS (L1, L2)

Gerald L. Condon

Sam Wilson

Johnson Space Center / Aeroscience and Flight Mechanics Division

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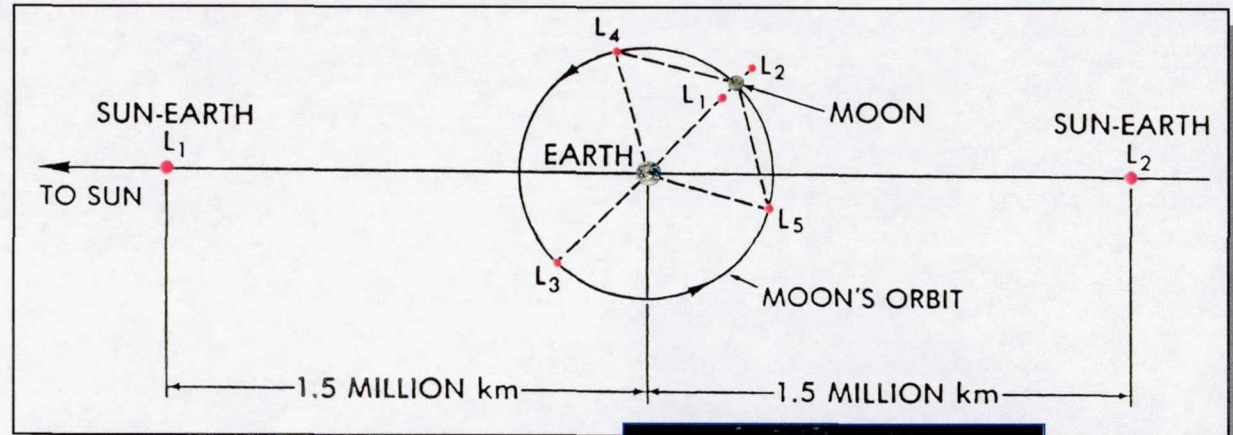
*October 9, 2002*



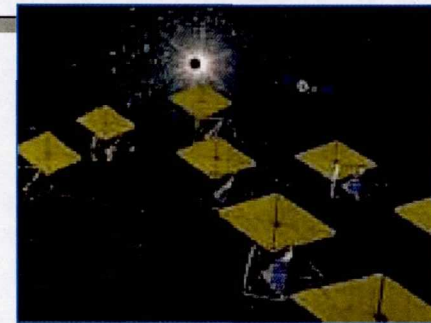


## Libration Point Missions

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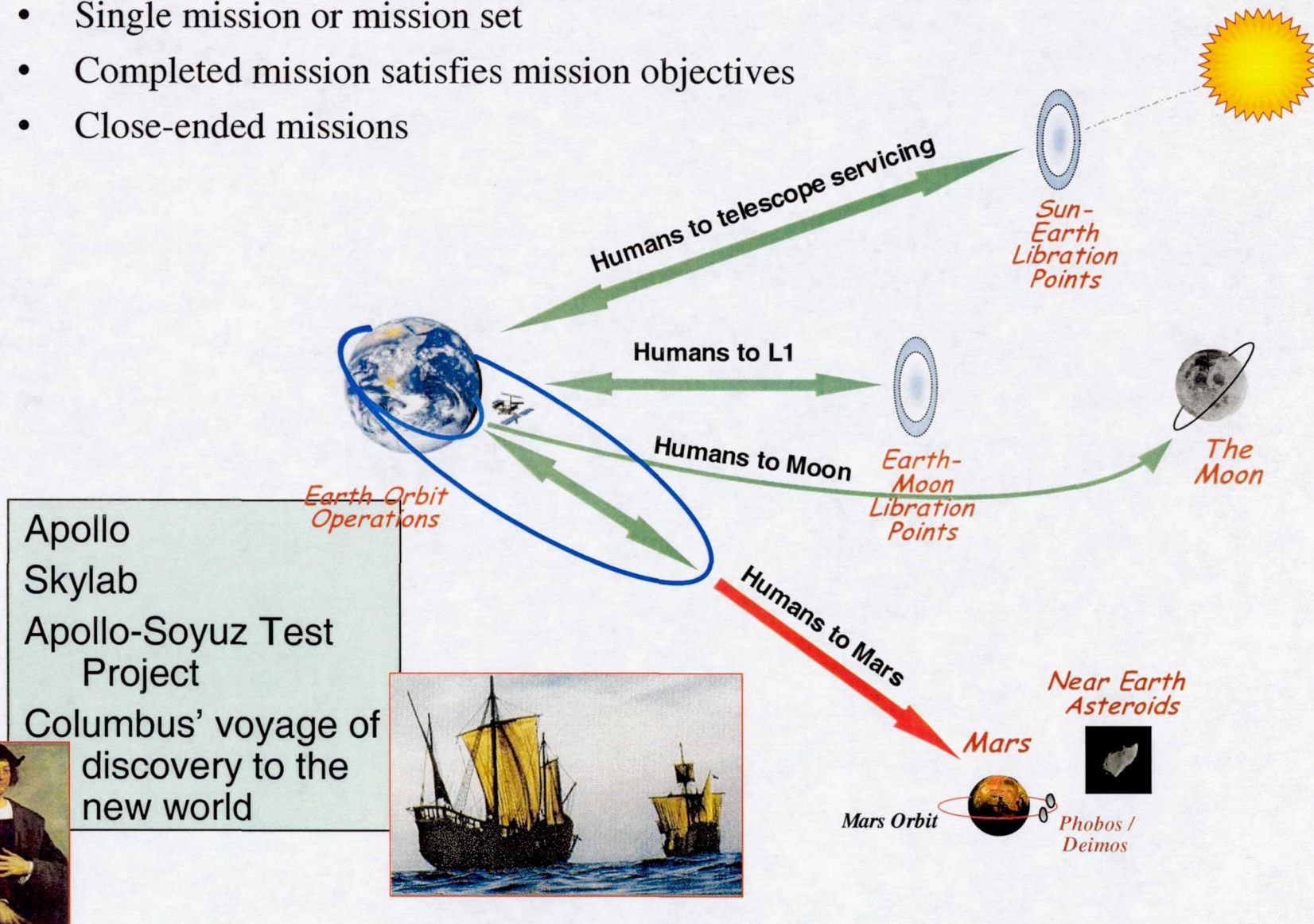
- Earth-Moon L1
  - Gateway station
    - Sorties to the Moon
    - Satellite deploy, servicing
      - Next Generation Space Telescope
      - Terrestrial Planet Finder
    - Staging area for interplanetary and asteroid missions
- Earth-Moon L2
  - Robotic relay satellites
    - Communications relay
    - Navigation aid
- Sun-Earth L2
  - Human missions to extend human presence in space





# Expeditionary vs. Evolutionary

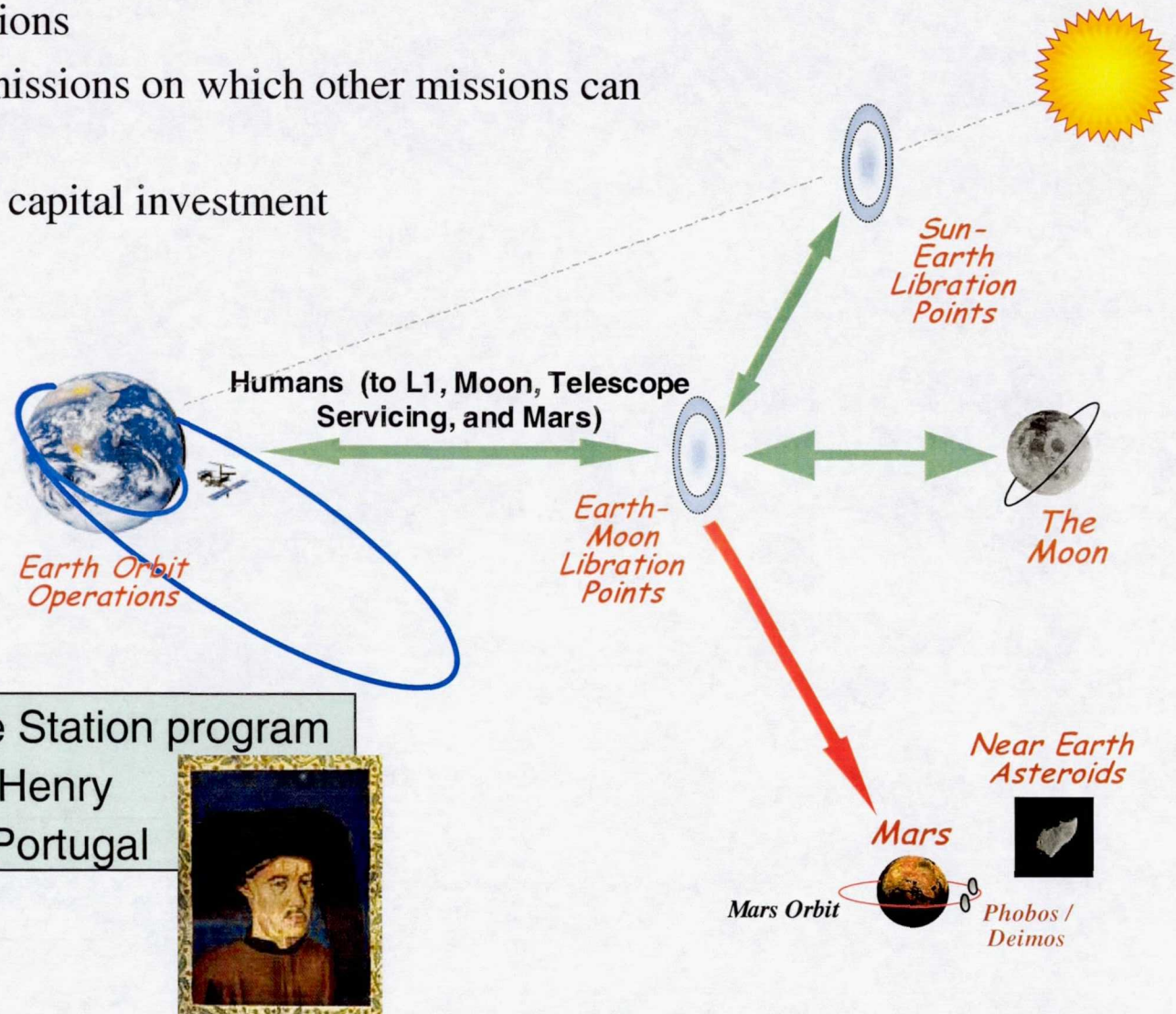
- Single mission or mission set
- Completed mission satisfies mission objectives
- Close-ended missions





# Expeditionary vs. Evolutionary

- Ongoing missions
- Open-ended missions on which other missions can build
- Greater initial capital investment

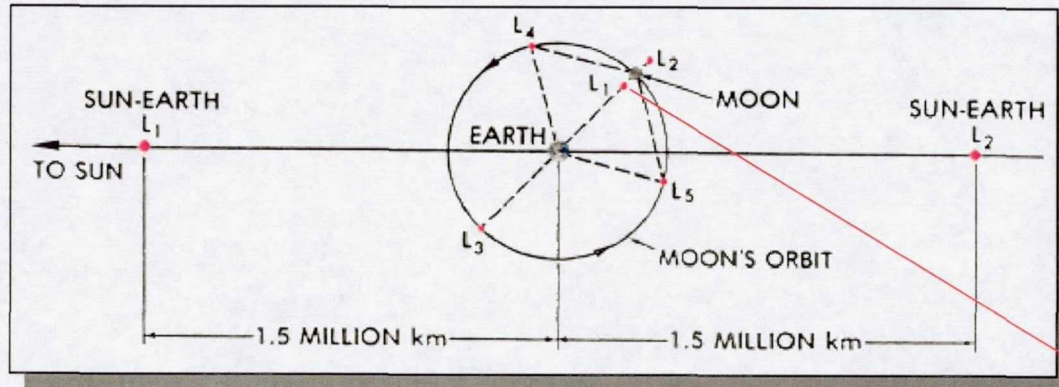


International Space Station program  
Voyages of Prince Henry  
the Navigator of Portugal

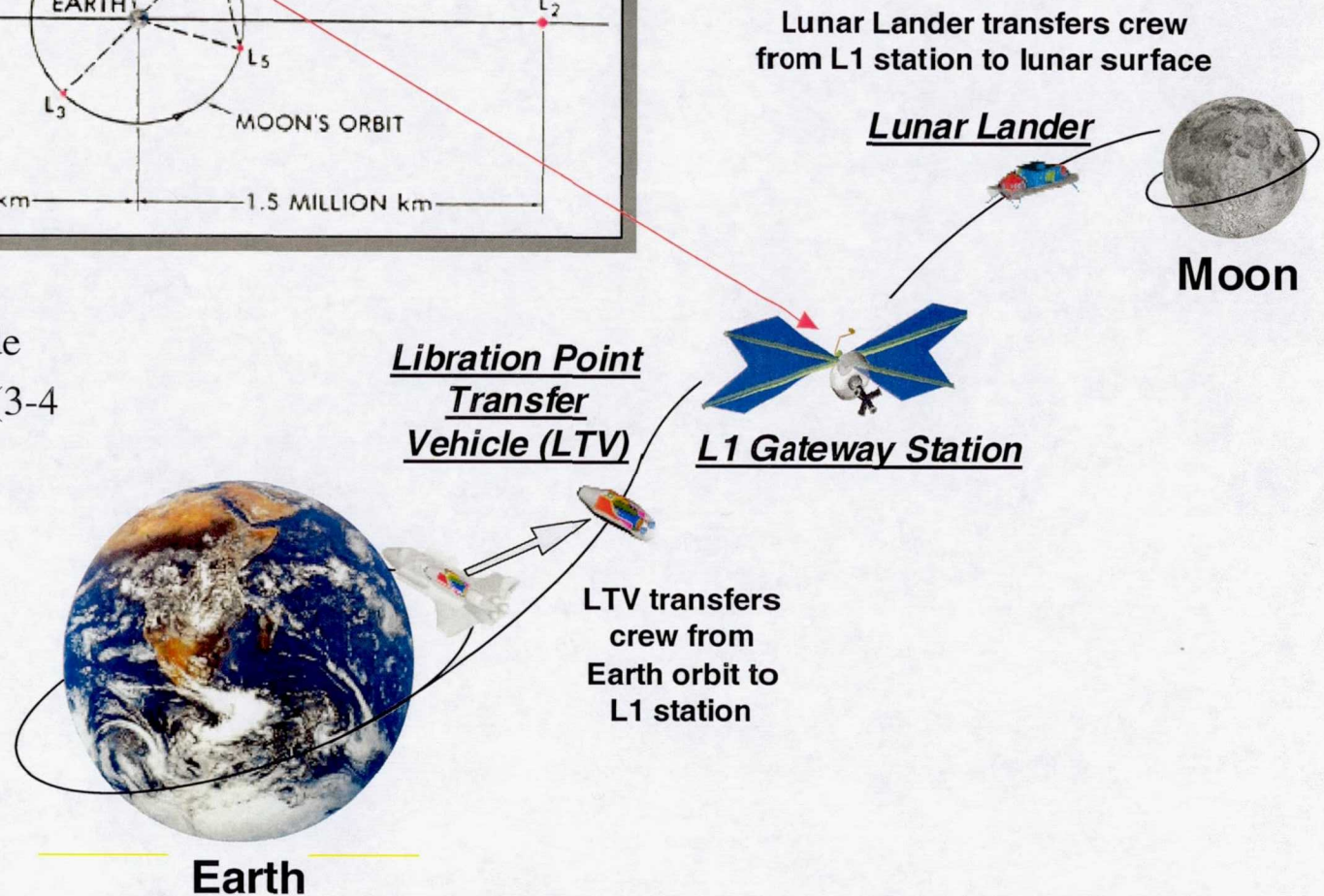




## Earth-Moon L1 – Gateway for Lunar Surface Operations

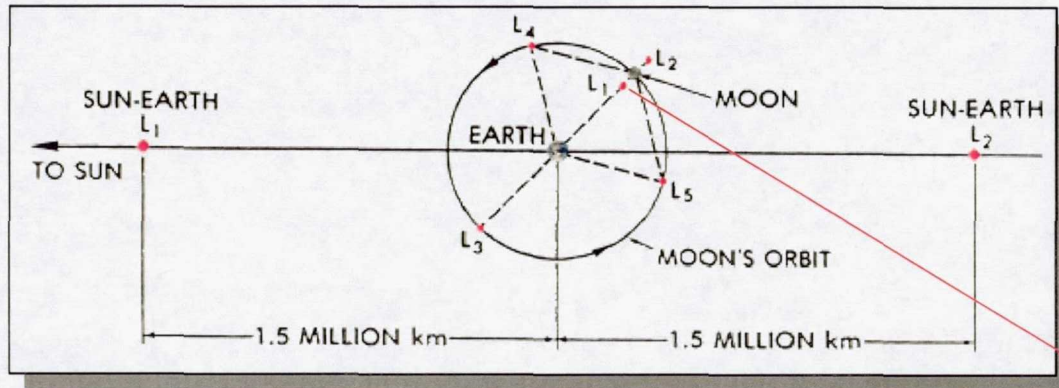


- Celestial park-n-ride
- Close to home (3-4 days)
- Staging to:
  - Moon

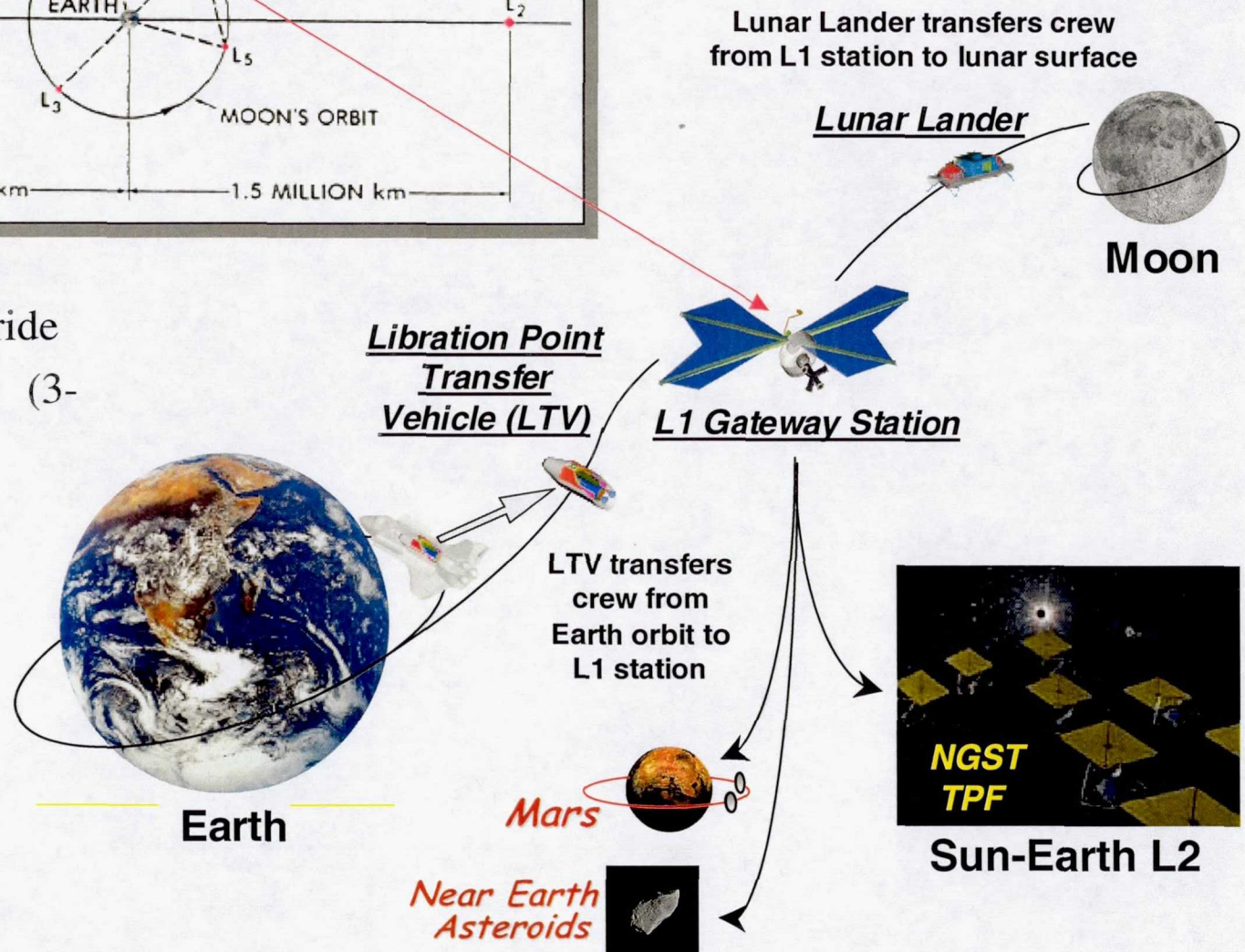




## Earth-Moon L1 – Gateway for Lunar Surface Operations



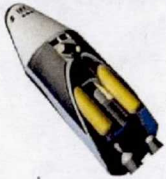
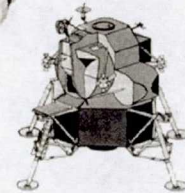
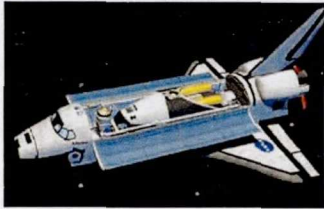
- Celestial park-n-ride
- Close to home (3-4 days)
- Staging to:
  - Moon
  - Sun-Earth L2
  - Mars
  - Asteroids
  - ...





## Lunar Mission: Libration Point vs. LOR

### Mission Scenario Advantages



#### Earth-Moon L1

- No lunar departure injection window
- Global lunar access
- Reusability
- Protection from failed station-keeping
- Specialized vehicle design

#### Lunar Orbit Rendezvous (LOR)

- Shorter mission duration
- Lower overall  $\Delta V$  cost
- Fewer critical maneuvers required





*JSC*

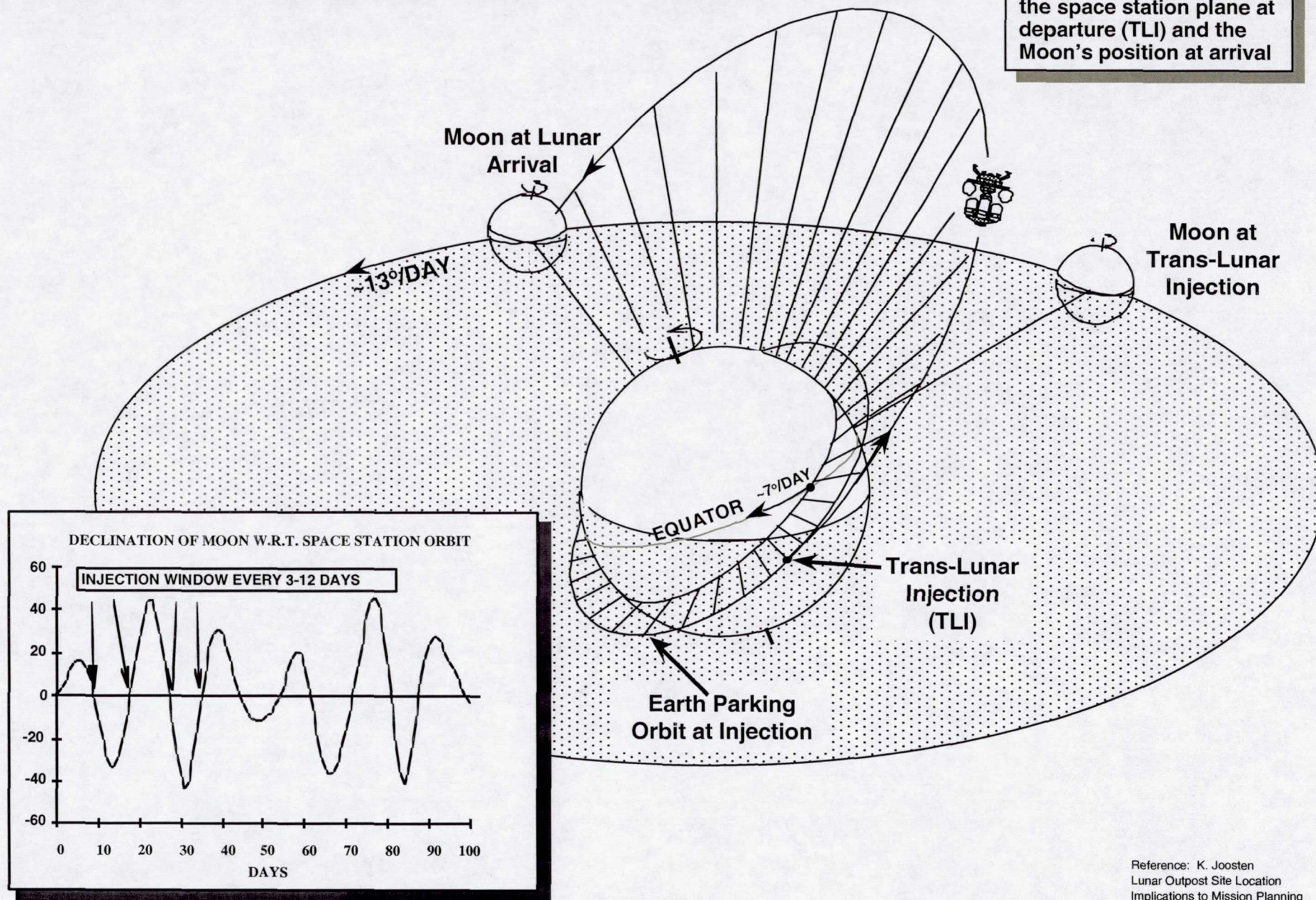
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# **Lunar Transfer/Orbit Diagrams**



## Trans-Lunar Trajectory from ISS Parking Orbit

TLI plane determined by the space station plane at departure (TLI) and the Moon's position at arrival





## Trans-Earth Trajectories

Moon at Trans-Earth Injection (TEI)

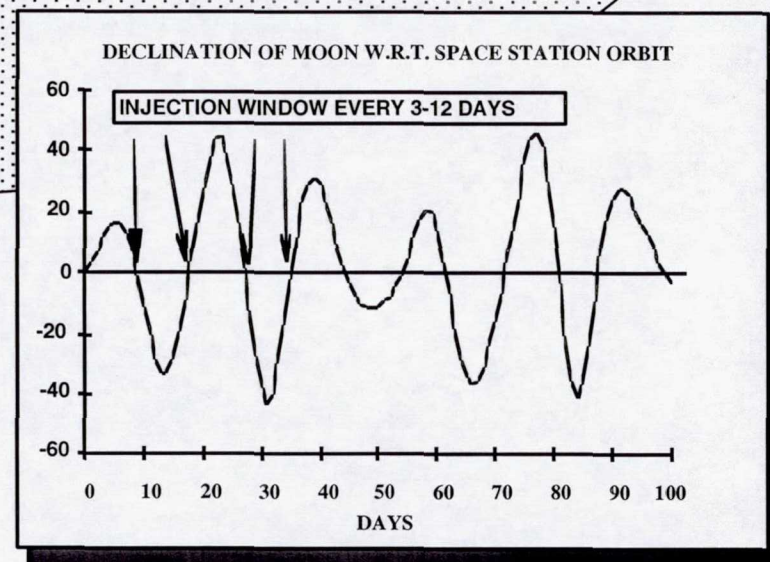
~13 deg/Day

Earth Parking Orbit

TEI plane determined by Moon's position at departure (TEI) and the space station plane at arrival

Earth Orbit Insertion

~7°/DAY  
EQUATOR

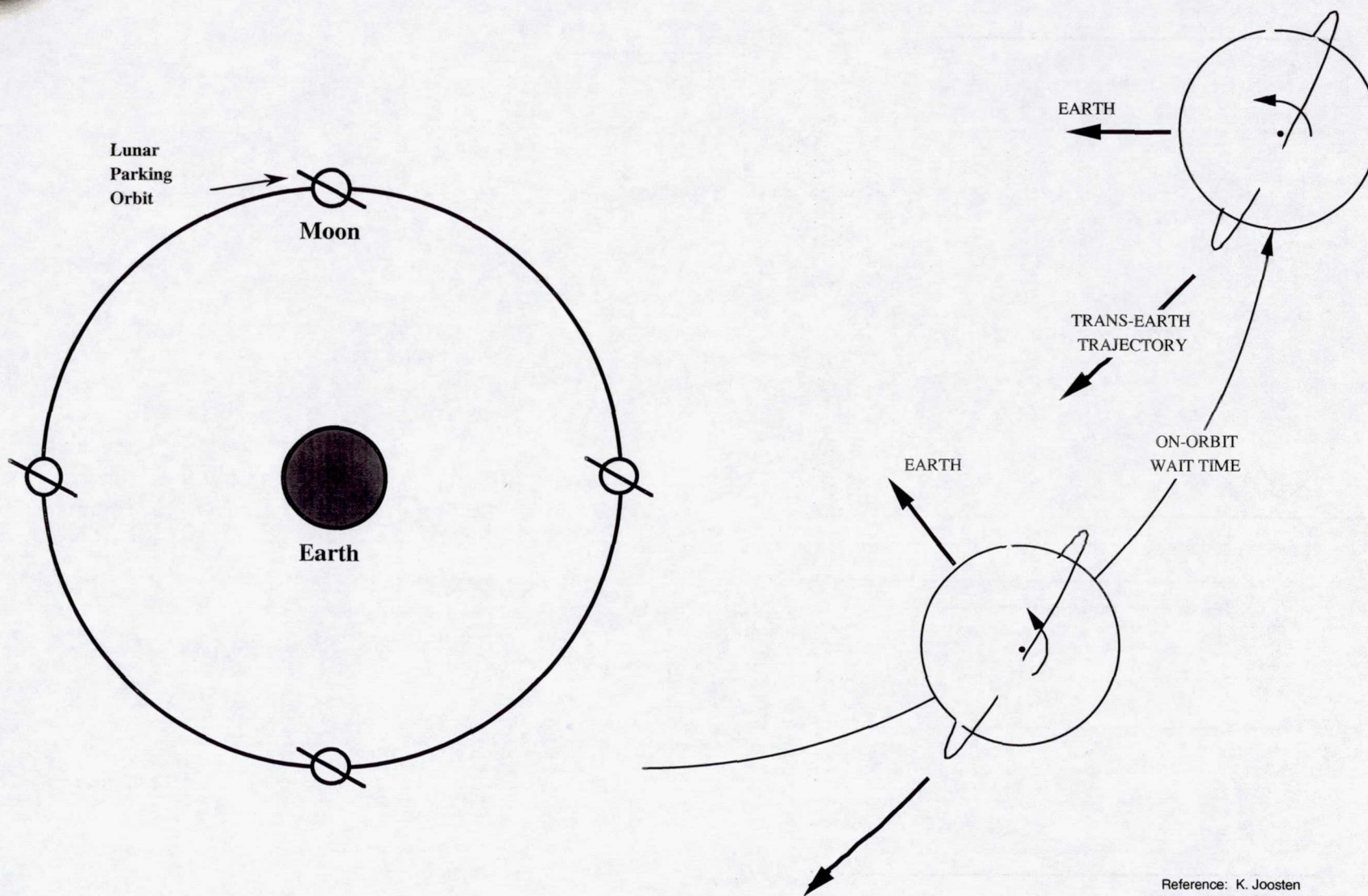






## Parking Orbit Considerations

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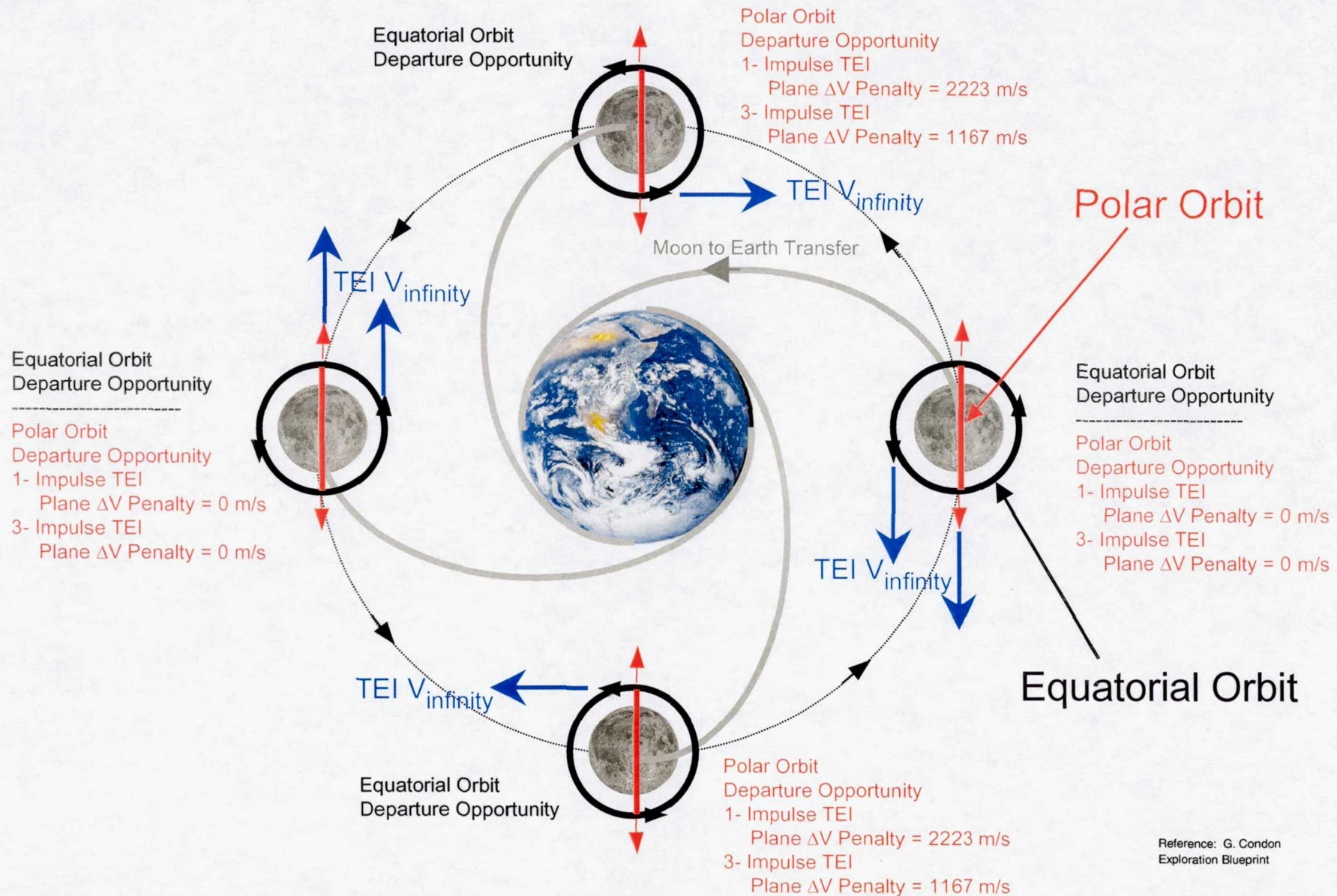


Reference: L. Wagner

Reference: K. Joosten  
Lunar Outpost Site Location  
Implications to Mission Planning

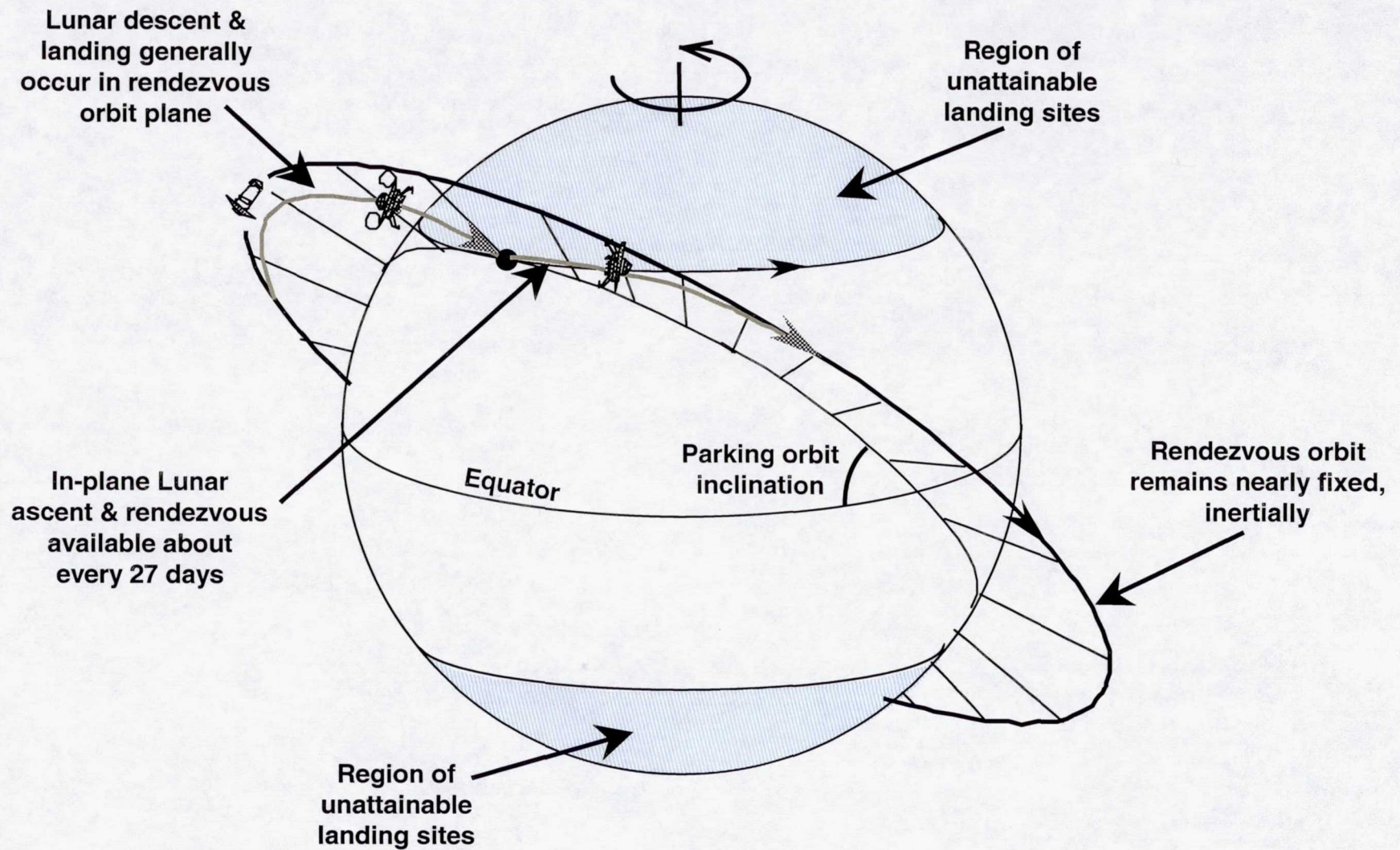


# Effect of Lunar Parking Orbit Inclination on Lunar Transfer Opportunities → Moon to Earth Transfer





## Landing Latitude Restrictions







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*Comparison of  
Opposition Class (Short-Stay) and  
Conjunction Class (Long-Stay)  
Missions for the Human Exploration of Mars*

Exploration Office

NASA/JSC

March 1998





# Mars Mission Planning

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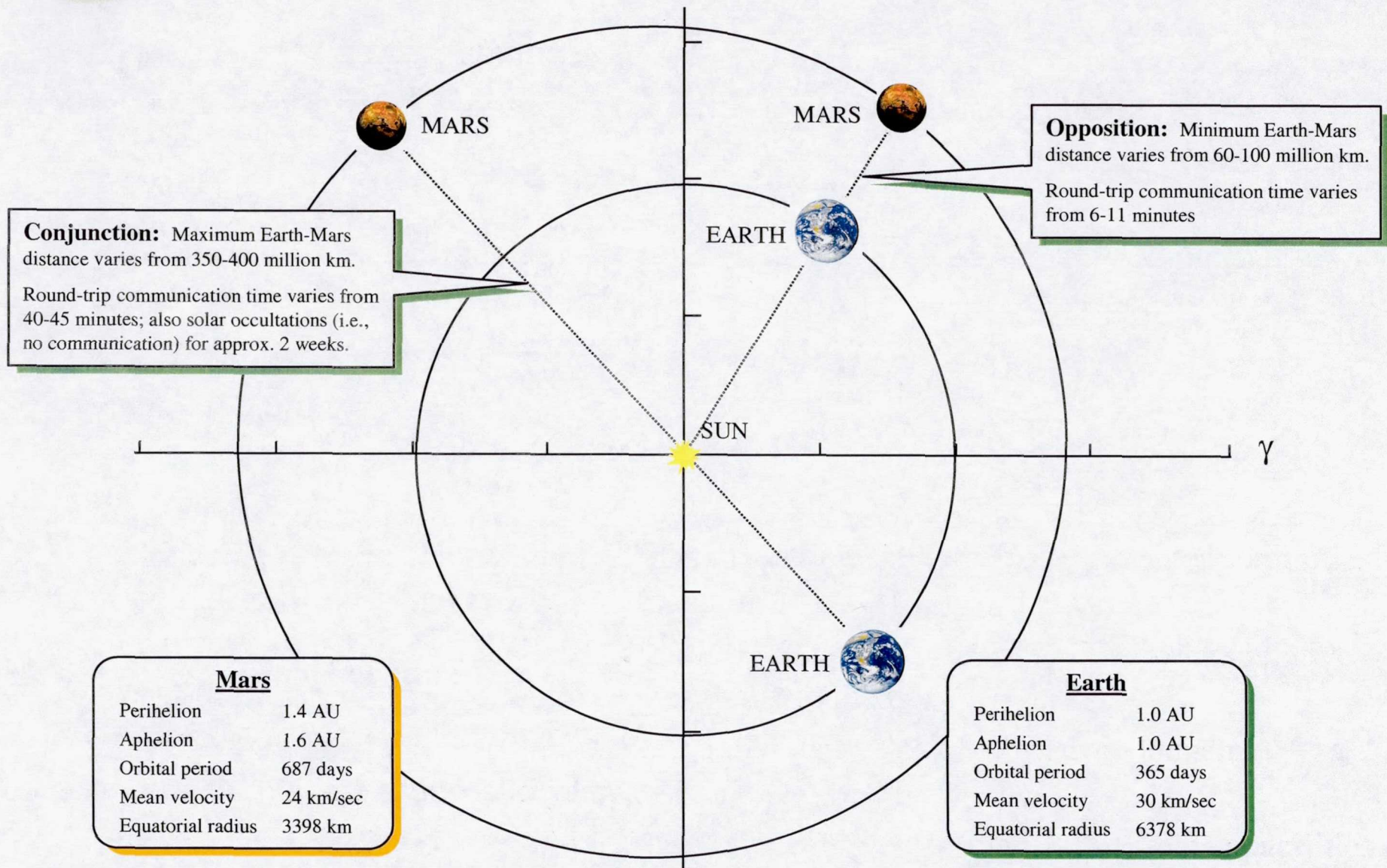
- Earth-Mars Mission Planning
  - Trips to Mars and back are, in effect, a double rendezvous problem
  - First rendezvous outbound must be developed considering influence of the rendezvous inbound
  - Practical considerations dictate favorable (and different) planetary alignments relative to the sun for both transfers
- Synodic Period
  - is the period of time necessary for the phase angle between Earth and Mars to repeat itself
  - Repetition rate for identical Earth-Mars phasing, and therefore launch opportunities for similar mission classes, is ~26 months
  - The eccentricity of Mars' orbit causes significant variations in Earth-Mars relative distance and velocity from one opportunity to the next
  - The entire range of Earth-Mars geometry is encompassed by seven launch opportunities, or about 15 years
  - Before definitive claims of mission characteristics or propulsion system capabilities are made, analysis across the 15-year cycle should be performed





# Earth-Mars Orbital Characteristics

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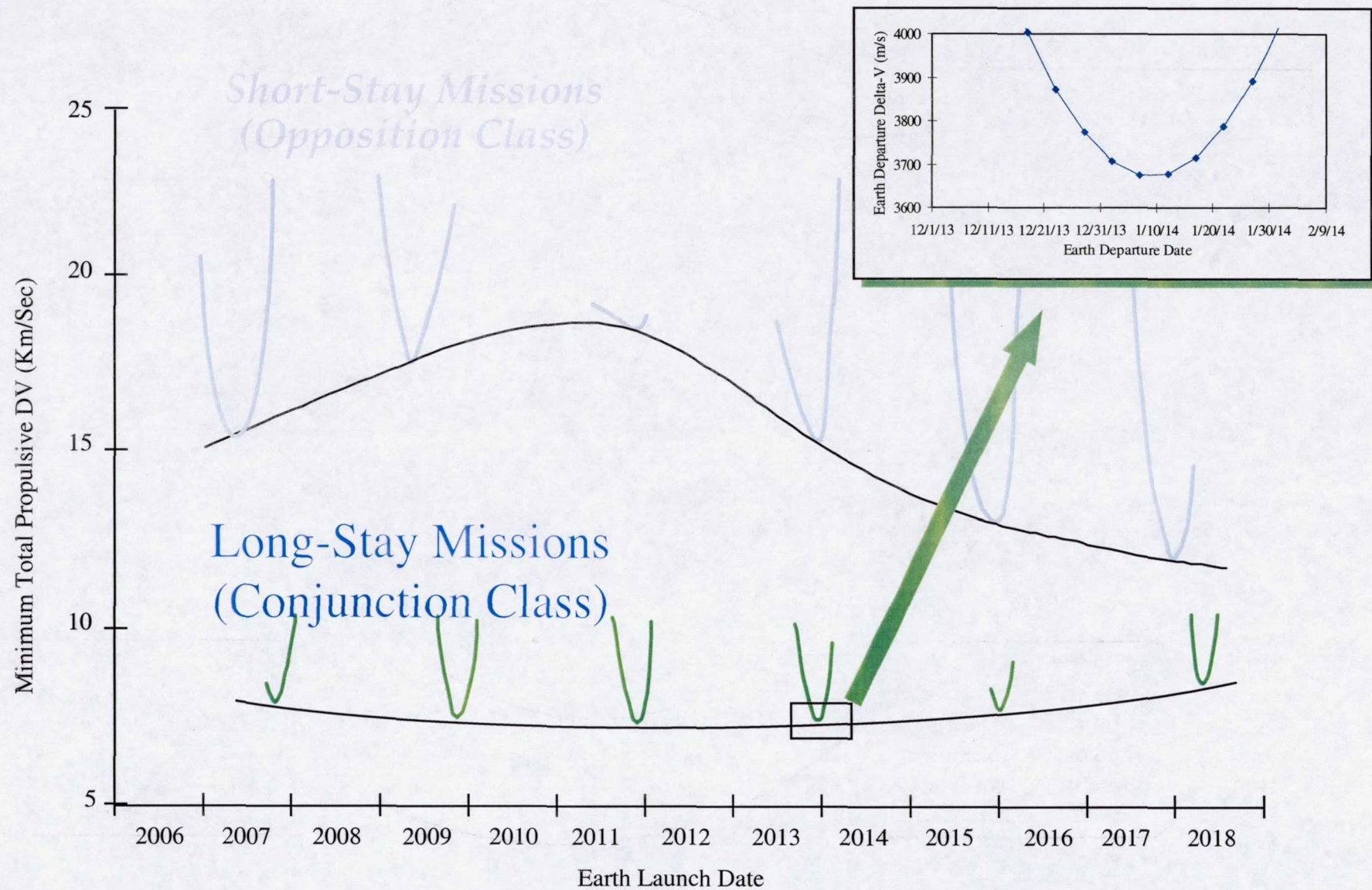






# Delta-V Variations

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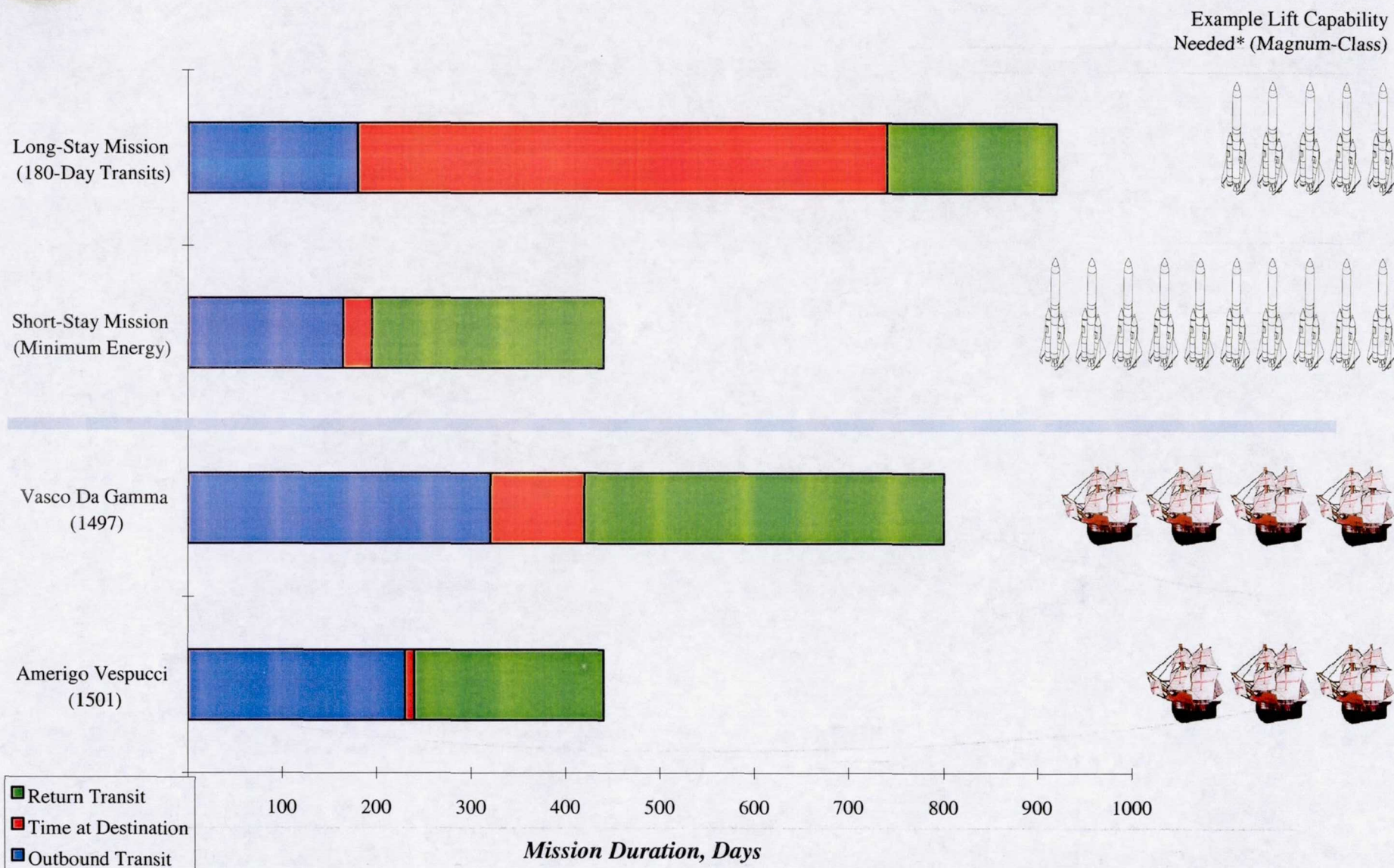






# Mars Mission Duration Comparison

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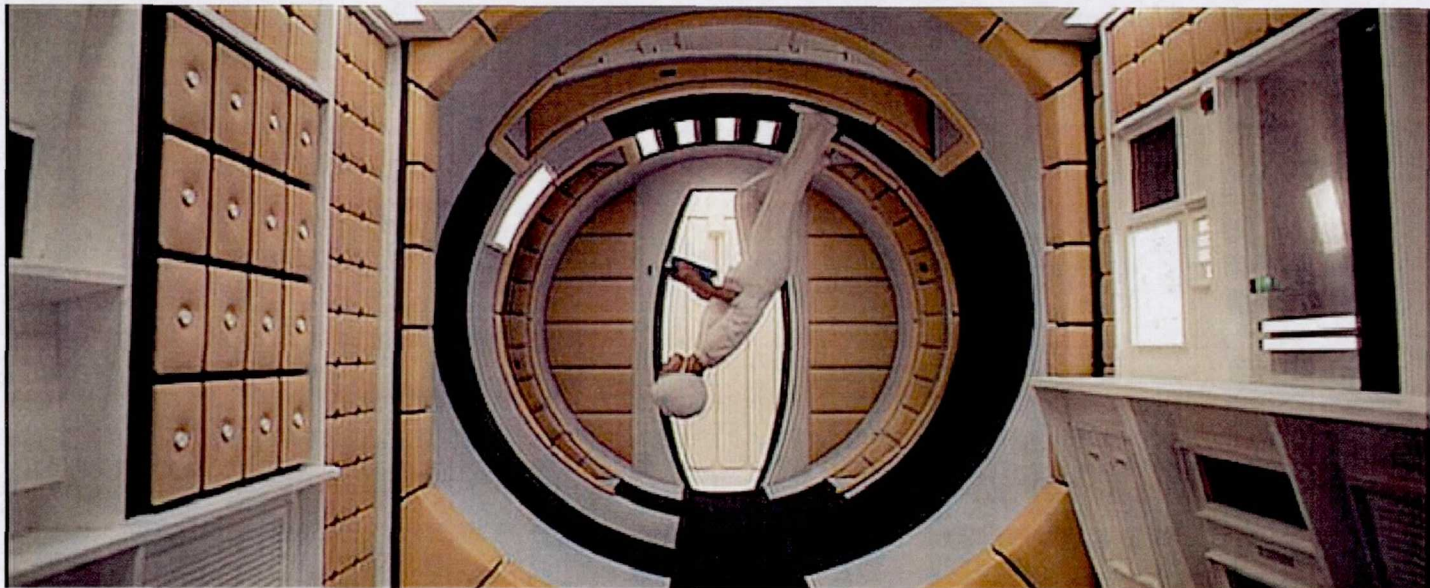
\* Assuming NTP=925 sec Propulsion





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## Artificial Gravity for Human Exploration Missions



### NEXT Status Report July 16, 2002

**B. KENT JOOSTEN**

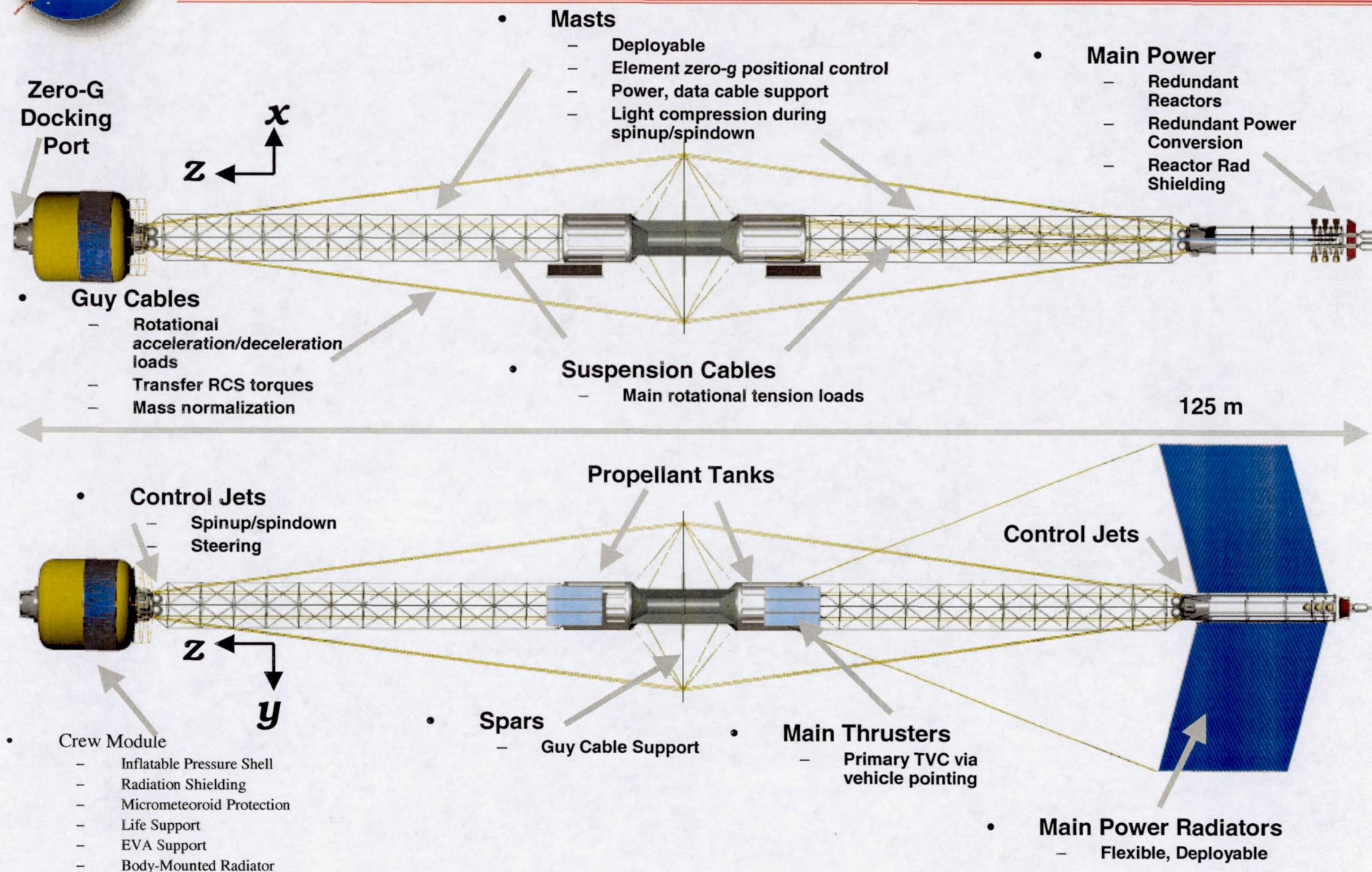
*Exploration Analysis and Integration Office*  
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
LYNDON B. JOHNSON SPACE CENTER  
2101 NASA Road 1, Houston, TX 77058-3696  
Mail Code: EX13 Voice: (281) 483-4645 FAX: (281) 244-7478  
[kent.joosten@jsc.nasa.gov](mailto:kent.joosten@jsc.nasa.gov)





## Current Configuration

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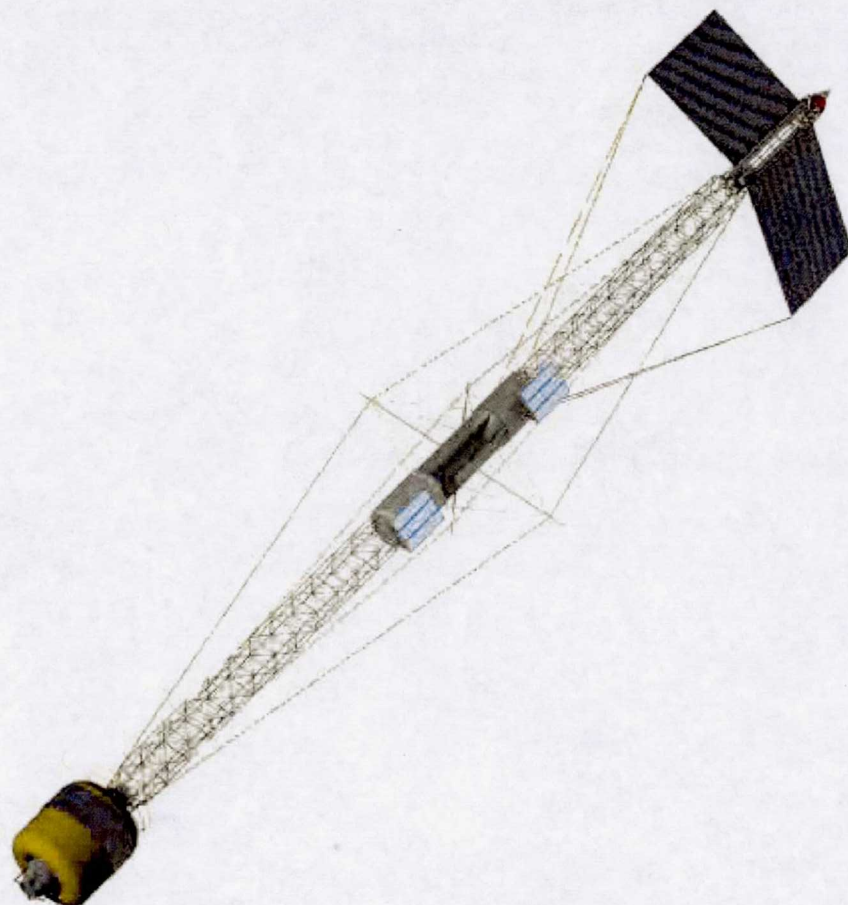






*JSC*

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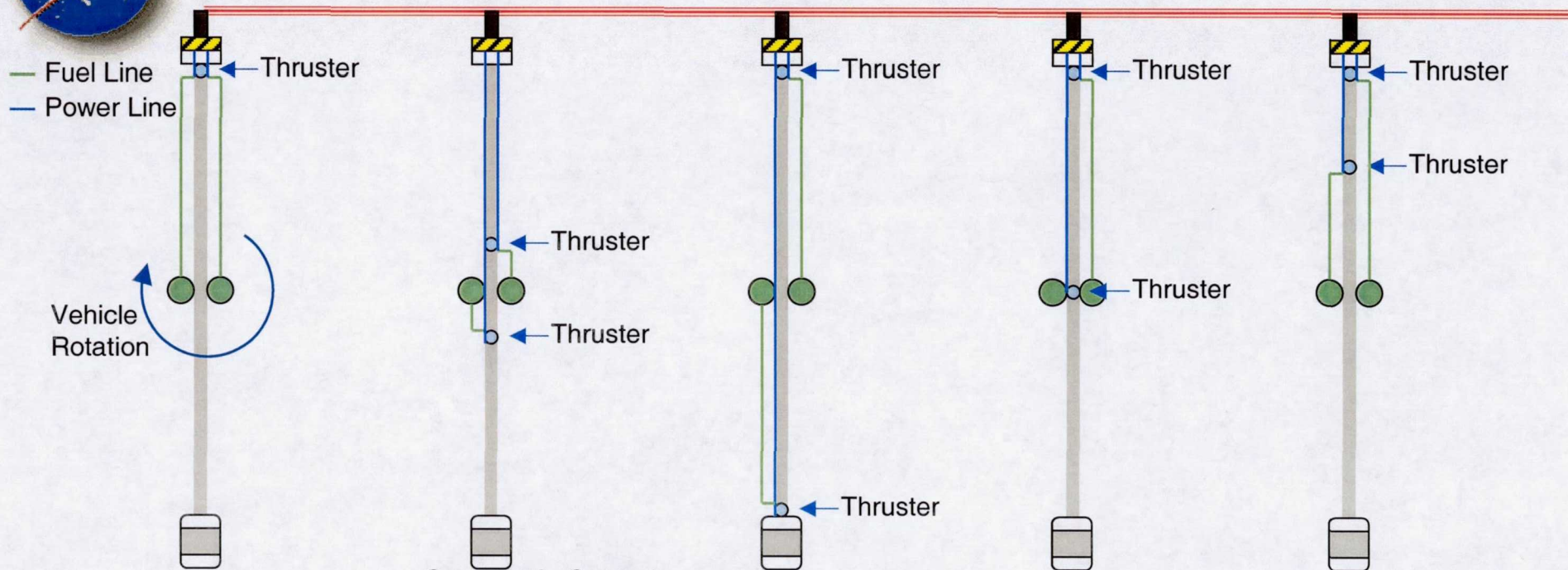






## NEP Thruster Location Trades

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	Original Asymmetric	Symmetric Central (Selected Config.)	Symmetric Terminal	Asymmetric CG	Asymmetric Counter
<b>Power Level*</b>	-- High Power Variation	+ Counter-cycling (near constant power)	+ Counter-cycling (near constant power)	+ Counter-cycling (near constant power)	+ Counter-cycling (near constant power)
<b>Power Lines</b>	+ Short power lines	-- Long power lines	-- Long power lines (no worse than previous)	-- Long power lines	+ Short power lines
<b>Prop Lines</b>	-- Long prop lines	+ Short prop lines	-- Long prop lines	-- Long prop lines	-- Long prop lines
<b>Turn Rates</b>	+ Higher turn rates	-- Lower turn rates	+ Best turn rates	+ Higher turn rates	-- Lower turn rates

\*For constant mass flow rate approach

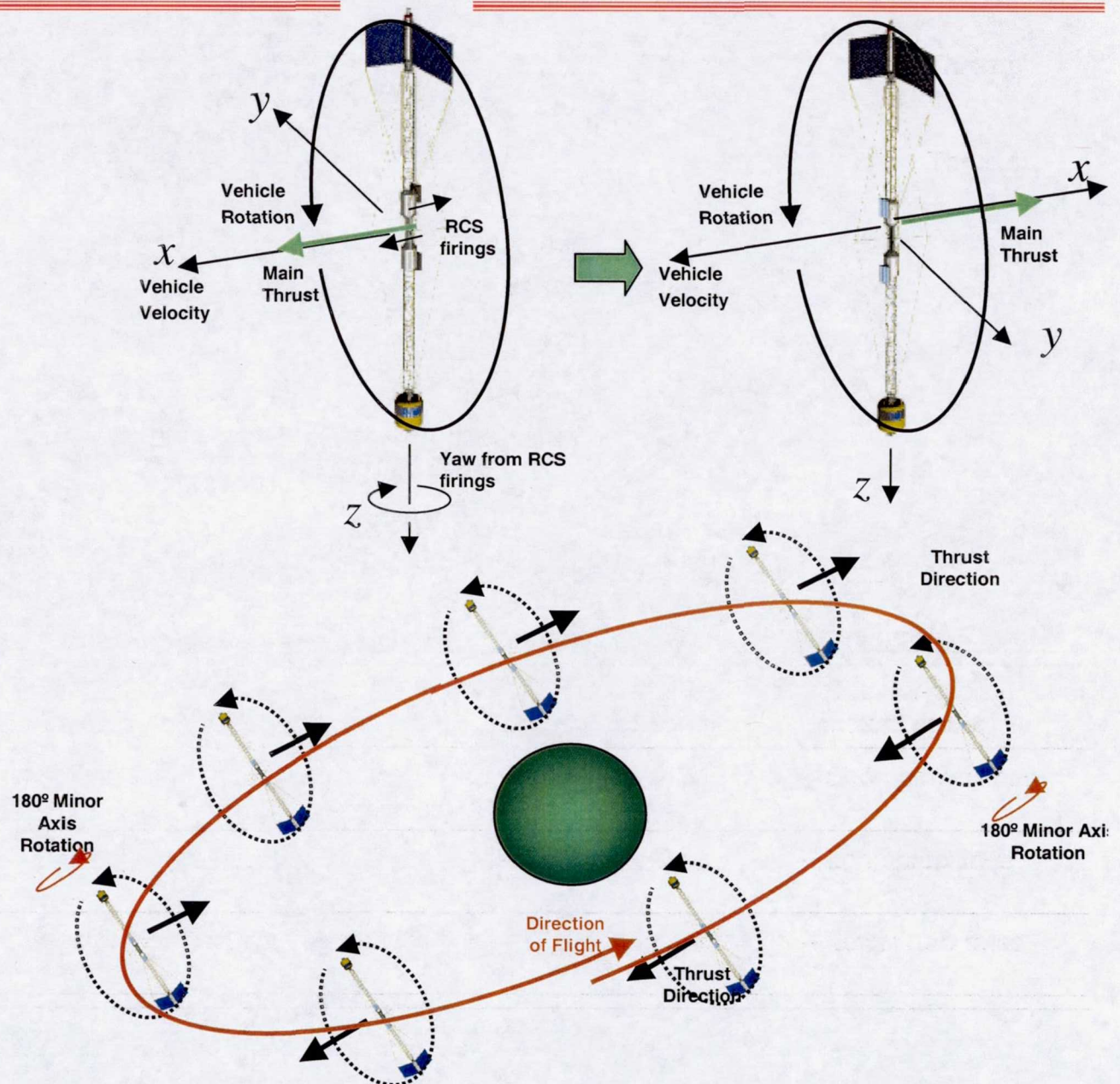




# Minor Axis Rotation

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- Technique for rotating thrust vector  $180^\circ$
- Rotation about vehicle z-axis
- Applications:
  - Midcourse turnaround
  - Planetary spirals (if required)
    - ~36% loss of propulsive efficiency vs. tangential thrusting
- Other possible implementation: second set of thrusters (-x thrust direction)
  - Thruster mass/expense vs. propellant required for rotation







# Example Load Paths (cont)

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- Mast loads for spinup, spindown
  - Mast will be under compression only during period when Hab Module/Power Module "weight" is less than compression load
    - Only mast loads identified to date
  - After that, no load (suspension cables support loads)
  - For spinup/down times less greater than 24 hours, compression loads will not exceed 100N (22 lbs)
  - Maximum mast loads may result from zero-g operations (hard to quantify at this time)
    - Docking forces
    - Plume impingements
- LaRC Analysis
  - Providing finite element modeling and analysis for load conditions
    - 1-g
    - Spinu/spindown
    - Maneuvers during transit
  - From loads analysis, determine low lightweight a structure (such as inflatabe/rigidizable structures) could be used for mast
  - Status
    - Modeling nearly complete
    - Analysis to begin shortly

Thrust Level, N	Spinup Time, hrs.	ArcJet Power, kWe	Guy Tension, N	Max. Mast Compression, N
5	100	65	24	23
10	50	131	47	46
15	33	196	71	70
20	25	262	95	93
25	20	327	119	116

ArcJet Computations Assume:  
Efficiency 30%  
Isp 800 sec

